# **RESEARCH ARTICLE**

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# Probabilistic Design of Helical Coil Spring for Longitudinal Invariance by Using Finite Element Method

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# ABSTRACT

The study represents new approach to design helical coil spring. Response surface modeling and analysis of open coiled helical spring by considering longitudinal and invariance have been carried out. Design parameters are wire diameter, spring diameter, height, number of turns elastic modulus in X and Z direction, poissions ratio, force. Simple equations is proposed which gives value of compressive stress of helical coil spring by carrying out regression analysis. It is observed that force and material property are significant parameters which affect compressive stress because their P value is 1. Relationship among design parameters and compressive stress has been obtained.

Key words: - Simulation, open coiled spring by FEA and Response surface modeling

## I. INTRODUCTION

Spring act as a flexible joint in between two parts or bodies. Spring is the energy storing and releasing element whenever required. This paper demonstrates by taking the combination of steel and composite material for design of helical compression spring. In this case instead of steel is used combination of steel and composite material Glass fiber/Epoxy because of low stiffness of single composite spring, which limits its application to light weight vehicle only. Composite material is light weight and corrosion resistance, it can withstand high temperature. It increase efficiency of vehicle and overcome the cost. He had concluded combination of steel and composite material can increase the stiffness which is the major requirement of regular vehicle due to higher weight this done by using the FEA.[1].This study investigates static behavior of helical structure under axial loads. In this paper, authors have taken two helical structure first one is single wire on which homogeneous theory applied and second is axial elastic properties of seven wire strand are computed. This approach, based on expansion, gives asymptotic the first-order approximation of the 3D elasticity problem from the solution of a 2D microscopic problem posed on the cross-section and a 1D macroscopic problem, which turns out to be a Navier-Bernoulli-Saint-Venant beam problem and result compared with reference results.[2]This paper researchers taken four composite material (structure)these are unidirectional laminates (AU), rubber core unidirectional laminates (UR), Unidirectional laminates with braided outer layer (BU), and rubber core unidirectional laminates with braided outer layer (BUR). They investigated

effect of rubber core and braided outer layer on the mechanical properties of the above mentioned helical springs. According to the experimental results, the helical composite spring with a rubber core can increase its failure load in compression by about 12%; while the spring with a braided outer layer cannot only increase its failure load in compression by about 18%, but also improve the spring constant by approximately 16%.[3]This study deals with the stress analysis of a helical coil compression spring, which is employed in three wheeler's auto-rickshaw belonging to the medium segment of the Indian automotive market. This spring has to face very high working stresses, so in this design of the spring both the elastic characteristics and the fatigue strength have to be considered as significant aspects. This done by using finite element analysis. These springs have to face very high working stresses. The structural reliability of the spring must therefore be ensured. [4]. The linear zed disturbance equations governing the resonant frequencies of a helical spring subjected to a static axial compressive load are solved numerically using the transfer matrix method for clamped ends and circular cross-section to produce frequency design charts. This paper summarize the behavior of the lowest resonant frequency obtained from the model of a helical compression spring with an initial number of turns.[5]In this paper, long term fatigue test on shot peened compression spring were conducted by means of special spring fatigue testing machine at 40 Hz. Three different types of material is taken.

The influence of different shot peening conditions were investigated. In this paper fractured test spring were examined under scanning electron microscope, optical microscope and by means of metallographic micro section in order to analyze the fracture behavior and the failure mechanisms [6].

It is observed from literature review that probabilistic approach for the design of helical coil spring by using FEA is not taken into consideration. Also probabilistic design by considering longitudinal invariance, Translational and combined translation plus longitudinal invariance is necessary to consider for design under dynamic loading condition. Validation of the analysis will be done by analytical techniques in finite element method or solid mechanics. Also results of probabilistic design are to be optimized. Results will provide new approach and key to improve design of helical coil spring.

### II. SIMULATION Finite element analysis of helical coil spring

Analysis has been carried out in ANSYS work bench. Constrained geometry of the spring is as shown in figure 1.1.



Fig.1.1 Geometry of the spring in ANSYS

In table No. 1.1 Simulation of helical coil spring is done by using response surface modeling in ANSYS workbench (FEA). Geometry is meshed by using brick element. Total number of nodes 25620 and elements 4850 are generated after meshing. One end of the spring is fixed in all direction while load is applied in negative Y direction at another end. It is shown in figure 1.2

In the table No. 1.2, material properties and their values in x, y, z direction is quoted.



Fig.1.2 Meshed model of helical coil spring

Table 1.1Material properties of spring for analysis

| Sr.No. | Material Property                               | Value |
|--------|---|-------|
| 1      | Young's modulus (EX),<br>MPa                    | 200e3 |
| 2      | Young's modulus ((EY)<br>MPa                    | 210e3 |
| 3      | Young's modulus (EZ) MPa                        | 220e3 |
| 4      | Shear modulus along XY-<br>direction (Gxy), MPa | 2433  |
| 5      | Shear modulus along XY-<br>direction (Gyz), MPa | 1698  |
| 6      | Shear modulus along XY-<br>direction (Gzx), MPa | 2433  |
| 7      | Force on x direction, N                         | 1000  |
| 8      | Poisson ratio along XY-<br>direction (NUxy)     | 0.3   |
| 9      | Poisson ratio along YZ-<br>direction (NUyz      | 0.27  |
| 10     | Poisson ratio along ZX-<br>direction (NUzx)     | 0.24  |

 Table 1.2 Limits of input parameter

| Sr.<br>No. | Parameters            | Lower<br>Limits | Higher<br>Limits |
|------------|-----------------------|-----------------|------------------|
| 1          | Height(mm)            | 50              | 55               |
| 2          | Wire diameter(mm)     | 4               | 5                |
| 3          | Turns(mm)             | 4               | 5                |
| 4          | Coil diameter(mm)     | 27              | 32               |
| 5          | Ez (MPa)              | 190e3           | 220e3            |
| 6          | Ex (MPa)              | 180e3           | 210e3            |
| 7          | Force Y Component (N) | 1000            | 1500             |

Table 1.1 shows material properties in X, Y and Z directions which are used for analysis. In table 1.2, lower and upper limit of input parameters are specified for uniform distribution

Simulation of helical coil spring is done by using response surface modeling in ANSYS workbench (FEA).

Table 1.3 shows corresponding parameters according to RSM. In this table,

P1 - Height, P2 – Wire diameter, P3 - Turns, P4 – Coil diameter, P5 - Young's Modulus Z direction (Pa), P6 - Young's Modulus X direction (Pa), P7 -Force Y Component (N), P8 - Equivalent Stress Maximum (Pa), P9 - Total Deformation Maximum (mm).

| Sr.No. | P1      | P2     | P3     | P4      | P5          | P6          | P7         | P8         | P9      |
|--------|---------|--------|--------|---------|-------------|-------------|------------|------------|---------|
| 1      | 50      | 5      | 5      | 30      | 211000      | 200000      | -1000      | 4737845097 | 0.37953 |
| 2      | 45      | 5      | 5      | 30      | 211000      | 200000      | -1000      | 4735321402 | 0.37454 |
| 3      | 55      | 5      | 5      | 30      | 211000      | 200000      | -1000      | 4737660972 | 0.38499 |
| 4      | 50      | 4.5    | 5      | 30      | 211000      | 200000      | -1000      | 6795865785 | 0.57608 |
| 5      | 50      | 5.5    | 5      | 30      | 211000      | 200000      | -1000      | 3604871584 | 0.26014 |
| 6      | 50      | 5      | 4.5    | 30      | 211000      | 200000      | -1000      | 5054538189 | 0.34210 |
| 7      | 50      | 5      | 5.5    | 30      | 211000      | 200000      | -1000      | 4991907953 | 0.41728 |
| 8      | 50      | 5      | 5      | 27      | 211000      | 200000      | -1000      | 4304231724 | 0.28213 |
| 9      | 50      | 5      | 5      | 33      | 211000      | 200000      | -1000      | 5172052972 | 0.49755 |
| 10     | 50      | 5      | 5      | 30      | 189900      | 200000      | -1000      | 4737845097 | 0.37953 |
| 11     | 50      | 5      | 5      | 30      | 232100      | 200000      | -1000      | 4737845097 | 0.37953 |
| 12     | 50      | 5      | 5      | 30      | 211000      | 180000      | -1000      | 4737845097 | 0.37953 |
| 13     | 50      | 5      | 5      | 30      | 211000      | 220000      | -1000      | 4737845097 | 0.37953 |
| 14     | 50      | 5      | 5      | 30      | 211000      | 200000      | -1100      | 5211629607 | 0.41748 |
| 15     | 50      | 5      | 5      | 30      | 211000      | 200000      | -900       | 4264060587 | 0.34157 |
| 16     | 47.3546 | 4.7355 | 4.7355 | 28.4127 | 199836.2096 | 189418.2081 | -947.0910  | 5004640196 | 0.37429 |
| 17     | 52.6454 | 4.7355 | 4.7355 | 28.4127 | 199836.2096 | 189418.2081 | -1052.9090 | 5566299912 | 0.42324 |
| 18     | 47.3546 | 5.2645 | 4.7355 | 28.4127 | 199836.2096 | 189418.2081 | -1052.9090 | 4091668192 | 0.27328 |
| 19     | 52.6454 | 5.2645 | 4.7355 | 28.4127 | 199836.2096 | 189418.2081 | -947.0910  | 3682079657 | 0.25001 |
| 20     | 47.3546 | 4.7355 | 5.2645 | 28.4127 | 199836.2096 | 189418.2081 | -1052.9090 | 5570176371 | 0.42749 |
| 21     | 52.6454 | 4.7355 | 5.2645 | 28.4127 | 199836.2096 | 189418.2081 | -947.0910  | 5011795224 | 0.39027 |
| 22     | 47.3546 | 5.2645 | 5.2645 | 28.4127 | 199836.2096 | 189418.2081 | -947.0910  | 3678421953 | 0.25266 |
| 23     | 52.6454 | 5.2645 | 5.2645 | 28.4127 | 199836.2096 | 189418.2081 | -1052.9090 | 4091586505 | 0.28508 |
| 24     | 47.3546 | 4.7355 | 4.7355 | 31.5873 | 199836.2096 | 189418.2081 | -1052.9090 | 6137490974 | 0.56183 |
| 25     | 52.6454 | 4.7355 | 4.7355 | 31.5873 | 199836.2096 | 189418.2081 | -947.0910  | 5527656778 | 0.51235 |
| 26     | 47.3546 | 5.2645 | 4.7355 | 31.5873 | 199836.2096 | 189418.2081 | -947.0910  | 4048357399 | 0.33194 |
| 27     | 52.6454 | 5.2645 | 4.7355 | 31.5873 | 199836.2096 | 189418.2081 | -1052.9090 | 4502311707 | 0.37429 |
| 28     | 47.3546 | 4.7355 | 5.2645 | 31.5873 | 199836.2096 | 189418.2081 | -947.0910  | 5524162900 | 0.52009 |
| 29     | 52.6454 | 4.7355 | 5.2645 | 31.5873 | 199836.2096 | 189418.2081 | -1052.9090 | 6162062321 | 0.58576 |
| 30     | 47.3546 | 5.2645 | 5.2645 | 31.5873 | 199836.2096 | 189418.2081 | -1052.9090 | 4505197410 | 0.37981 |
| 31     | 52.6454 | 5.2645 | 5.2645 | 31.5873 | 199836.2096 | 189418.2081 | -947.0910  | 4053577500 | 0.34588 |
| 32     | 47.3546 | 4.7355 | 4.7355 | 28.4127 | 222163.7904 | 189418.2081 | -1052.9090 | 5563805484 | 0.41611 |
| 33     | 52.6454 | 4.7355 | 4.7355 | 28.4127 | 222163.7904 | 189418.2081 | -947.0910  | 5006883760 | 0.38070 |
| 34     | 47.3546 | 5.2645 | 4.7355 | 28.4127 | 222163.7904 | 189418.2081 | -947.0910  | 3680453400 | 0.24581 |
| 35     | 52.6454 | 5.2645 | 4.7355 | 28.4127 | 222163.7904 | 189418.2081 | -1052.9090 | 4093476174 | 0.27794 |
| 36     | 47.3546 | 4.7355 | 5.2645 | 28.4127 | 222163.7904 | 189418.2081 | -947.0910  | 5010370704 | 0.38452 |
| 37     | 52.6454 | 4.7355 | 5.2645 | 28.4127 | 222163.7904 | 189418.2081 | -1052.9090 | 5571760200 | 0.43388 |
| 38     | 47.3546 | 5.2645 | 5.2645 | 28.4127 | 222163.7904 | 189418.2081 | -1052.9090 | 4089409783 | 0.28089 |
| 39     | 52.6454 | 5.2645 | 5.2645 | 28.4127 | 222163.7904 | 189418.2081 | -947.0910  | 3680379765 | 0.25643 |
| 40     | 47.3546 | 4.7355 | 4.7355 | 31.5873 | 222163.7904 | 189418.2081 | -947.0910  | 5520669811 | 0.50537 |
| 41     | 52.6454 | 4.7355 | 4.7355 | 31.5873 | 222163.7904 | 189418.2081 | -1052.9090 | 6145258487 | 0.56959 |
| 42     | 47.3546 | 5.2645 | 4.7355 | 31.5873 | 222163.7904 | 189418.2081 | -1052.9090 | 4500677927 | 0.36902 |
| 43     | 52.6454 | 5.2645 | 4.7355 | 31.5873 | 222163.7904 | 189418.2081 | -947.0910  | 4049826914 | 0.33667 |
| 44     | 47.3546 | 4.7355 | 5.2645 | 31.5873 | 222163.7904 | 189418.2081 | -1052.9090 | 6141374347 | 0.57820 |
| 45     | 52.6454 | 4.7355 | 5.2645 | 31.5873 | 222163.7904 | 189418.2081 | -947.0910  | 5542771793 | 0.52689 |
| 46     | 47.3546 | 5.2645 | 5.2645 | 31.5873 | 222163.7904 | 189418.2081 | -947.0910  | 4052422635 | 0.34164 |
| 47     | 52.6454 | 5.2645 | 5.2645 | 31.5873 | 222163.7904 | 189418.2081 | -1052.9090 | 4506481409 | 0.38452 |
| 48     | 47.3546 | 4.7355 | 4.7355 | 28.4127 | 199836.2096 | 210581.7919 | -1052.9090 | 5563805484 | 0.41611 |
| 49     | 52.6454 | 4.7355 | 4.7355 | 28.4127 | 199836.2096 | 210581.7919 | -947.0910  | 5006883760 | 0.38070 |
| 50     | 47.3546 | 5.2645 | 4.7355 | 28.4127 | 199836.2096 | 210581.7919 | -947.0910  | 3680453400 | 0.24581 |
| 51     | 52.6454 | 5.2645 | 4.7355 | 28.4127 | 199836.2096 | 210581.7919 | -1052.9090 | 4093476174 | 0.27794 |
| 52     | 47.3546 | 4.7355 | 5.2645 | 28.4127 | 199836.2096 | 210581.7919 | -947.0910  | 5010370704 | 0.38452 |
| 53     | 52.6454 | 4.7355 | 5.2645 | 28.4127 | 199836.2096 | 210581.7919 | -1052.9090 | 5571760200 | 0.43388 |

# Table No.1.3 Corresponding parameters according to RSM (Response Surface Modelling)

Continued

|    |         |        |        |         |             |             |            |            | Continued |
|----|---------|--------|--------|---------|-------------|-------------|------------|------------|-----------|
| 54 | 47.3546 | 5.2645 | 5.2645 | 28.4127 | 199836.2096 | 210581.7919 | -1052.9090 | 4089409783 | 0.28089   |
| 55 | 52.6454 | 5.2645 | 5.2645 | 28.4127 | 199836.2096 | 210581.7919 | -947.0910  | 3680379765 | 0.25643   |
| 56 | 47.3546 | 4.7355 | 4.7355 | 31.5873 | 199836.2096 | 210581.7919 | -947.0910  | 5520669811 | 0.50537   |
| 57 | 52.6454 | 4.7355 | 4.7355 | 31.5873 | 199836.2096 | 210581.7919 | -1052.9090 | 6145258487 | 0.56959   |
| 58 | 47.3546 | 5.2645 | 4.7355 | 31.5873 | 199836.2096 | 210581.7919 | -1052.9090 | 4500677927 | 0.36902   |
| 59 | 52.6454 | 5.2645 | 4.7355 | 31.5873 | 199836.2096 | 210581.7919 | -947.0910  | 4049826914 | 0.33667   |
| 60 | 47.3546 | 4.7355 | 5.2645 | 31.5873 | 199836.2096 | 210581.7919 | -1052.9090 | 6141374347 | 0.57820   |
| 61 | 52.6454 | 4.7355 | 5.2645 | 31.5873 | 199836.2096 | 210581.7919 | -947.0910  | 5542771793 | 0.52689   |
| 62 | 47.3546 | 5.2645 | 5.2645 | 31.5873 | 199836.2096 | 210581.7919 | -947.0910  | 4052422635 | 0.34164   |
| 63 | 52.6454 | 5.2645 | 5.2645 | 31.5873 | 199836.2096 | 210581.7919 | -1052.9090 | 4506481409 | 0.38452   |
| 64 | 47.3546 | 4.7355 | 4.7355 | 28.4127 | 222163.7904 | 210581.7919 | -947.0910  | 5004640196 | 0.37429   |
| 65 | 52.6454 | 4.7355 | 4.7355 | 28.4127 | 222163.7904 | 210581.7919 | -1052.9090 | 5566299912 | 0.42324   |
| 66 | 47.3546 | 5.2645 | 4.7355 | 28.4127 | 222163.7904 | 210581.7919 | -1052.9090 | 4091668192 | 0.27328   |
| 67 | 52.6454 | 5.2645 | 4.7355 | 28.4127 | 222163.7904 | 210581.7919 | -947.0910  | 3682079657 | 0.25001   |
| 68 | 47.3546 | 4.7355 | 5.2645 | 28.4127 | 222163.7904 | 210581.7919 | -1052.9090 | 5570176371 | 0.42749   |
| 69 | 52.6454 | 4.7355 | 5.2645 | 28.4127 | 222163.7904 | 210581.7919 | -947.0910  | 5011795224 | 0.39027   |
| 70 | 47.3546 | 5.2645 | 5.2645 | 28.4127 | 222163.7904 | 210581.7919 | -947.0910  | 3678421953 | 0.25266   |
| 71 | 52.6454 | 5.2645 | 5.2645 | 28.4127 | 222163.7904 | 210581.7919 | -1052.9090 | 4091586505 | 0.28508   |
| 72 | 47.3546 | 4.7355 | 4.7355 | 31.5873 | 222163.7904 | 210581.7919 | -1052.9090 | 6137490974 | 0.56183   |
| 73 | 52.6454 | 4.7355 | 4.7355 | 31.5873 | 222163.7904 | 210581.7919 | -947.0910  | 5527656778 | 0.51235   |
| 74 | 47.3546 | 5.2645 | 4.7355 | 31.5873 | 222163.7904 | 210581.7919 | -947.0910  | 4048357399 | 0.33194   |
| 75 | 52.6454 | 5.2645 | 4.7355 | 31.5873 | 222163.7904 | 210581.7919 | -1052.9090 | 4502311707 | 0.37429   |
| 76 | 47.3546 | 4.7355 | 5.2645 | 31.5873 | 222163.7904 | 210581.7919 | -947.0910  | 5524162900 | 0.52009   |
| 77 | 52.6454 | 4.7355 | 5.2645 | 31.5873 | 222163.7904 | 210581.7919 | -1052.9090 | 6162062321 | 0.58576   |
| 78 | 47.3546 | 5.2645 | 5.2645 | 31.5873 | 222163.7904 | 210581.7919 | -1052.9090 | 4505197410 | 0.37981   |

As shown in the table No.3.4. Regression analysis of helical coil spring is carried out by using M S excels 2014 for obtaining regression equation. Regression analysis of helical coil spring has been done by using M S excel and following equation of regression is obtained.

## **III. RESULTS AND DISCUSSION**

In this chapter, analysis of helical coil spring by using the response surface modeling has been discussed. This analysis provides the resulting graphs of design parameters Vs compressive stress. Under the loading condition, compression strength of helical coil spring is obtained. Stress distribution of helical coil spring is as shown below in figure 1.3.In this case, static analysis is done by using the finite element method, in the figure blue color indicates the minimum stresses 4.8343E6 acting on the turns and Red color indicates maximum stresses 4.7378E9. The force applied in y direction .Material properties in Y direction are kept constants i.e. longitudinal invariance while material properties in other two directions are varied within range 190e3 to 220e3.



Fig.1.3. Equivalent stress of helical coil spring

#### a) Coil diameter Vs Compressive stress

Figure shows relationship between coil diameter Vs compressive stress has been obtained. In this fig showing that when mean diameter of spring increases compressive stress also goes on increasing upto 32mm. There compressive stress decreases because stress exceeds elastic limit.



Fig.1.3. Mean diameter Vs Compressive stress





Figure shows young's modulus Vs compressive stress in this case, when young's modulus increase the compressive stress increases up to 210E3 after that compressive stress decrease up to upper limit i.e. 230E3 N/mm2. It happens due to high stiffness value ofspring.

#### c) Wire diameter Vs Compressive stress

Figure shows the wire diameter Vs compressive stress. When wire diameter of spring is increases compressive stress decreases up to 5mm after these compressive stress increase force is transferred in helical direction to another end of spring. From fig. it is observed that 5mm is optimum wire diameter where compressive stress is 4.8N/mm2



Wire dimeter(mm)

#### Fig.1.5. Wire diameter Vs Compressive stress



Fig.1.6. Force Vs Compressive stress

Figure shows graph of force Vs compressive stress. In this graph shown that when force increases compressive stress also increase, so compressive stress depend on applied force. From obtained regression model it is observed that force is one among significant parameter

## e) Free length Vs compressive stress

Figure shows graph of free length VS compressive stress. graph obtained shows exactly reverse nature as that of wire diameter Vs compressive stress. As shown in the fig. free length increases up to 50mm there after compressive stress decrease up to free length 55mm because energy stored in spring is released.



Fig.1.7. Free length Vs compressive stress

#### **IV CONCLUSION**

- Simple equations proposed which gives value of compressive stress of helical coil spring by carrying regression analysis
- It is observed that force and material property are significant parameters which affect compressive stress because their P value is 1.
- Finite element analysis of helical coil spring has been carried out.
- Response surface modeling of helical coil spring under longitudinal invariance has been carried out for compression stress.
- Relationship among design parameters and compressive stress has been obtained

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